

LECTURE

MODELLING THE MARINE ENVIRONMENT

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Lecture 7

PROCESS OF SUBSTANCE TRANSMISSION

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Lecture 7A

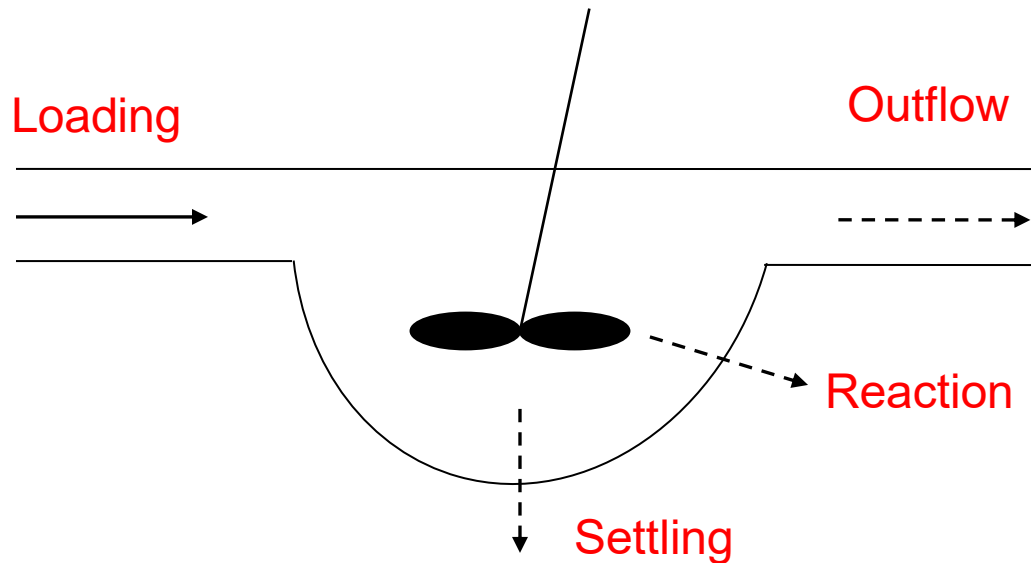
MASS BALANCING EQUATION

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ThS. Đặng Thị Thanh Lê*

- ❖ **MASS balancing equation**
- ❖ **Steady - state system Solution**
 - Transfer functions
 - Residence
- ❖ **Unsteady - state system Solution**
 - Impulse loading
 - Step loading
 - Linear loading
 - Exponential loading
 - Sinusoidal loading

MASS BALANCE FOR A WELL-MIXED LAKE

A completely mixing system. (CSTR – Continuously Stirred Tank Reactor)
It's the simplest system that can be used to model a real water body.



For a finite time period, the mass balance of the system is described by the equation:

$$\text{Accumulation} = \text{Loading} - \text{OutFlow} - \text{Reaction} - \text{Settling}$$

MASS BALANCE FOR A WELL-MIXED LAKE (Cont)

❖ **Accumulation:** represent the change of Mass M of the system over a period of time t .

$$\left. \begin{array}{l} \text{Accumulation} = \frac{\Delta M}{\Delta t} \\ c = \frac{M}{V} \rightarrow M = Vc \end{array} \right\} \rightarrow \text{Accumulation} = \frac{\Delta Vc}{\Delta t} \quad [MT^{-1}]$$

If V is constant

$$\text{Accumulation} = V \frac{\Delta c}{\Delta t} \rightarrow V \frac{dc}{dt}$$

$\frac{dc}{dt} > 0 \rightarrow$ Increased accumulation
 $\frac{dc}{dt} < 0 \rightarrow$ Reduced accumulation
 $\frac{dc}{dt} = 0 \rightarrow$ Constant

MASS BALANCE FOR A WELL-MIXED LAKE (cont)

❖ Loading :

$$\text{Loading} = W(t) = Qc_{\text{in}}(t) \quad [\text{MT}^{-1}]$$

Q : Flow [L^3T^{-1}]

$c_{\text{in}}(t)$: concentration [ML^{-3}]

❖ **Point source** (source identity, convenient measurement, continuity)

- + Municipal wastewater
- + Industrial wastewater
- + Tributary

❖ **Distribution source**

- Agriculture
- Atmosphere
- Water flowing from the city.
- Groundwater

MASS BALANCE FOR A WELL-MIXED LAKE (cont)

❖ Outflow:

- ❖ **A WELL-MIXED LAKE** : $c = c_{out}$
 $\rightarrow \text{Outflow} = Qc_{out} = Qc$

❖ Reaction:

$$\text{Reaction} = kM = kVc$$

k: First order reaction coefficient [T^{-1}]

❖ Settling:

$$\text{Settling} = vA_s c$$

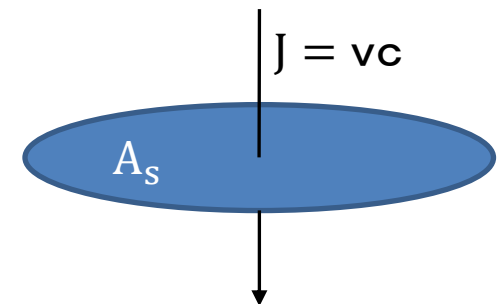
$$V = A_s H$$

$$\rightarrow \text{Settling} = \frac{v}{H} Vc = k_s Vc$$

v: apparent settling velocity [LT^{-1}]

k_s : a first – oder settling rate constant= v/H [T^{-1}]

H: depth[L]



MASS BALANCE FOR A WELL-MIXED LAKE (cont)

❖ Mass balancing equation

$$V \frac{dc}{dt} = W(t) - Qc - kVc - vA_s c$$

- Dependent variable: c
- Independent variable : t
- Impact function: $W(t)$, which represents external influence on the system
- Parameter: $V, Q, k, v, \text{ và } A_s$

MASS BALANCE FOR A WELL-MIXED LAKE (cont)

➤ Mass balance equation

$$V \frac{dc}{dt} = W(t) - Qc - kVc - vA_s c = 0$$

➤ Solution

$$c = \frac{W}{Q+kV+vA_s} \text{ hoặc } c = \frac{W}{a}$$

➤ Assimilation agent (self-cleansing ability)

$$a = Q + kV + vA_s$$

STEADY - SYSTEM SOLUTION(cont)

Example 1:

A lake has the following characteristics: volume = 50,000 m³, depth = 2m, inflow = outflow = 7500m³/day, temperature = 25⁰C. The lake receives the input of pollutants from three sources:

- a factory discharge of 50 kg/day
- a flux from the air with a load of 0.6 g/m²/day
- the inflow stream has a concentration of 10mg/l

If the pollutant decay at the rate of 0.25/day at 20⁰C ($\theta=1.05$).

a) Calculation of assimilation agents.

b) Determine the steady – state concentration

c) Calculates the mass per time for each term in the mass balance and displays your results on a plot.

STEADY - SYSTEM SOLUTION(cont)

❖ Transfer function

$$c = \frac{W}{Q + kV + vA_s} = \frac{Qc_{in}}{Q + kV + vA_s}$$
$$\rightarrow \frac{c}{c_{in}} = \beta = \frac{Q}{Q + kV + vA_s} : \text{Transfer function}$$

- Transfer function : it specified how the system input is transformed into an output
- $\beta \ll 1$: the mechanical cleaning of the lake will reduce the concentration of pollution (high assimilation capacity)
- $\beta \rightarrow 1$: weak lake cleaning mechanics

❖ Residence time

- ❖ The residence time of a substance E represents the mean amount of time that a particle of E would reside in a system.

$$\tau_E = \frac{E}{|dE/dt|_{\pm}}$$

E: Quantity of E in a specified volume [M or ML^{-3}]

$|dE/dt|_{\pm}$: absolute value of source or lake [MT^{-1} or $ML^{-3}T^{-1}$]

- The residence time of the water in the lake: $\tau = \frac{V}{Q}$
- The residence time of pollutants in the lake

$$\tau = \frac{Vc}{Qc + kVc + vA_s c} = \frac{V}{Q + kV + vA_s}$$

STEADY - SYSTEM SOLUTION(cont)

Example 2:

A lake has the following characteristics: volume = 50,000 m³, depth = 2m, inflow = outflow = 7500m³/day, temperature = 25⁰C. The lake receives the input of pollutants from three sources:

- a factory discharge of 50 kg/day
- a flux from the air with a load of 0.6 g/m²/day
- the inflow stream has a concentration of 10mg/l

If the pollutant decay at the rate of 0.25/day at 20⁰C ($\theta=1.05$).

- a) Inflow concentration.
- b) Transfer function
- c) The residence time of the water
- d) The residence time of pollutants

STEADY - SYSTEM SOLUTION(cont)

Exercises: A lake has the following characteristics.:

Surface area = $2 \times 10^5 \text{ m}^2$, Medium depth = 3 m, $Q_{\text{in}} = Q_{\text{out}} = 45000 \text{ m}^3/\text{day}$, inflow BOD concentration = 4 mg/l , residence time = 2 week

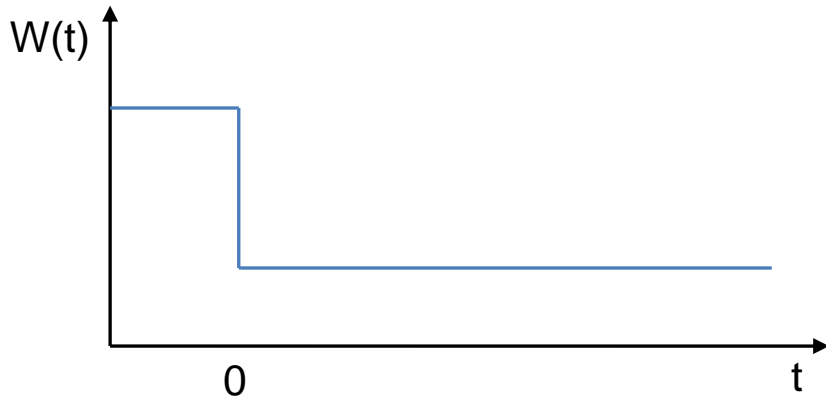
A subdivision housing 1 000 people will discharges raw sewage into this system. Individual contributes about

150 x 3.785 litter/day

and 0.25 x 453.6 g/day.

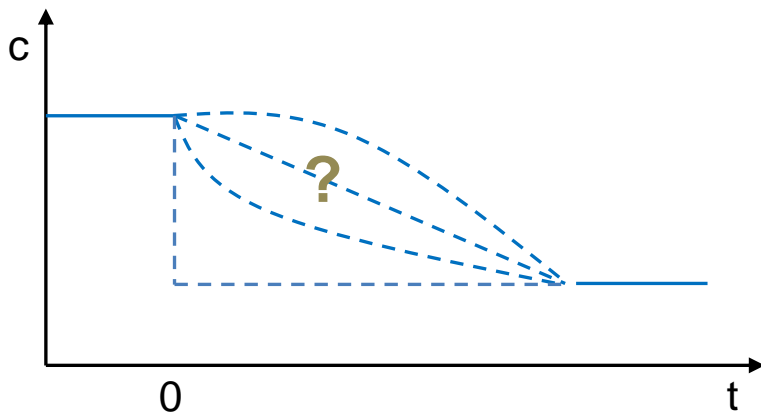
- Determine the BOD concentration of wastewater (mg/l).
- If BOD decay = 0.1 day^{-1} and settles at rate of 0.1 m/day. Calculate the assimilation factor for lake prior to building subdivision housing .
- Calculation of transfer function factor after subdivision housing.
- Determine the steady concentration of the lake in both cases with and without subdivision housing.

UNSTEADY- SYSTEMS SOLUTION (CONT)



At a certain point, if the reduction in pollutant emissions takes place, two questions will be asked as follows:

- How long will the water quality be restored?
- What is the "shape" of this recovery?



4 water quality recovery scenarios with reduced pollutant load

UNSTEADY- SYSTEMS SOLUTION (CONT)

To determine the path of pollutants, consider the equation of mass balance:

$$V \frac{dc}{dt} = W(t) - Qc - kVc - vA_s c$$

$$\Leftrightarrow \frac{dc}{dt} = \frac{W(t)}{V} - \frac{Q}{V}c - kc - \frac{v}{H}c$$

$$\Leftrightarrow \frac{dc}{dt} + \lambda c = \frac{W(t)}{V} \quad (*)$$

With $\lambda = \frac{Q}{V} + k + \frac{v}{H}$: eigenvalue

If Q, V, k, v, H is constant, equation (*) are differential equations, first order, linear, and heterogeneous. The solution consists of two parts:

$$c = c_g + c_p$$

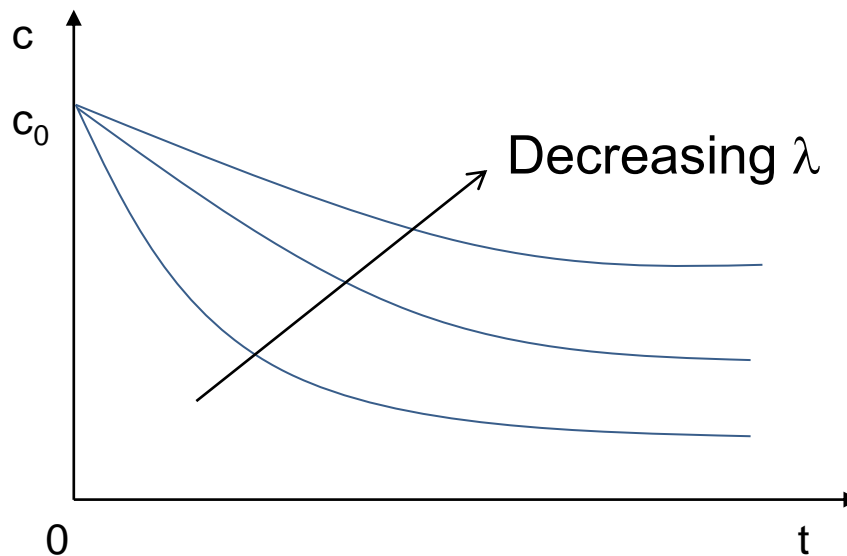
c_g : Generalized solution for the case $W(t) = 0$

c_p : particular solution for specified form $W(t)$

UNSTEADY- SYSTEMS SOLUTION (TT)

❖ General solution(c_g)

- $W(t) = 0$: $c = c_g$
- At $t = 0$: $c = c_0 \rightarrow$ solution of equation (*) is: $c = c_0 e^{-\lambda t}$



The temporal response of well – mixed
lake model following the termination of
all loading

UNSTEADY- SYSTEMS SOLUTION (CONT)

❖ Response time

- The time the lake needs to recover..
- t_ϕ = **Response time** $\phi\%$, which means the time it takes to achieve it.
 $\phi\%$ the final level of recovery of the lake..

$$t_\phi = \frac{1}{\lambda} \ln \frac{100}{100 - \phi}$$

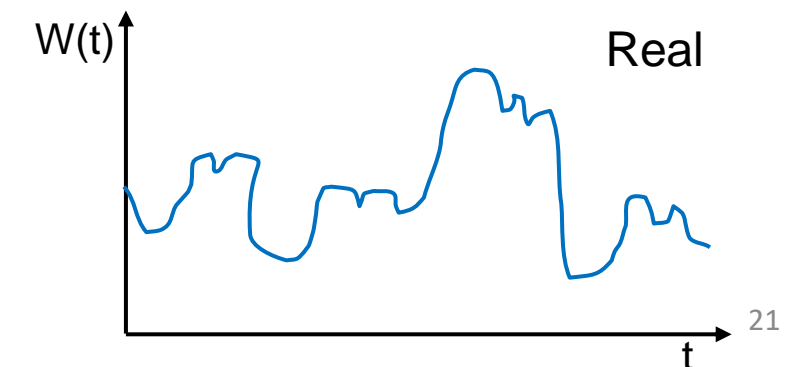
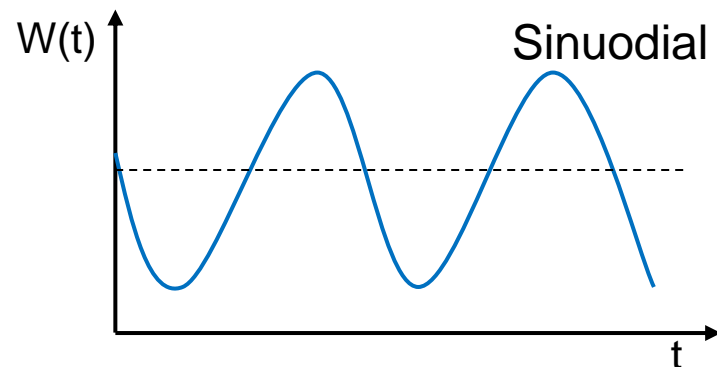
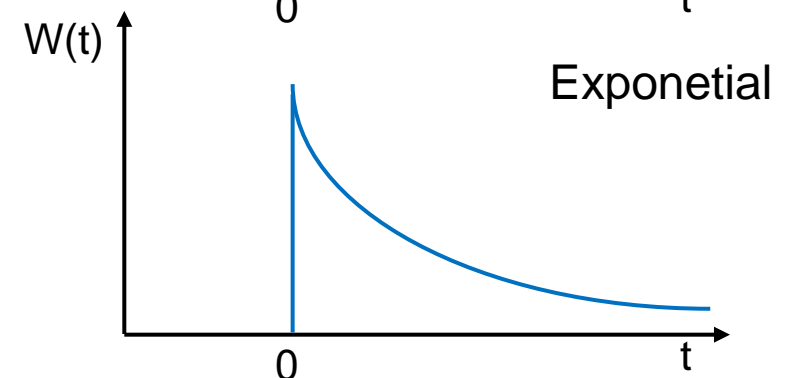
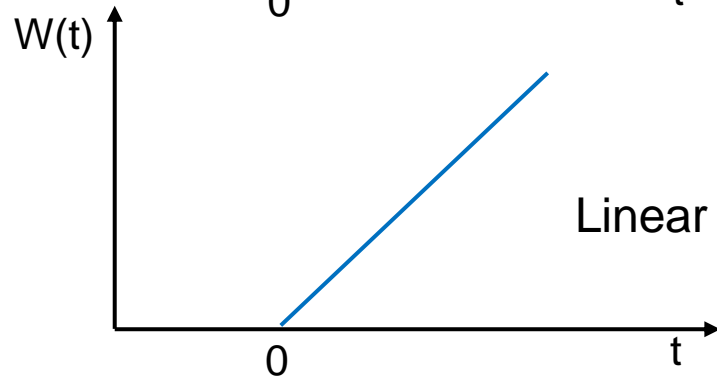
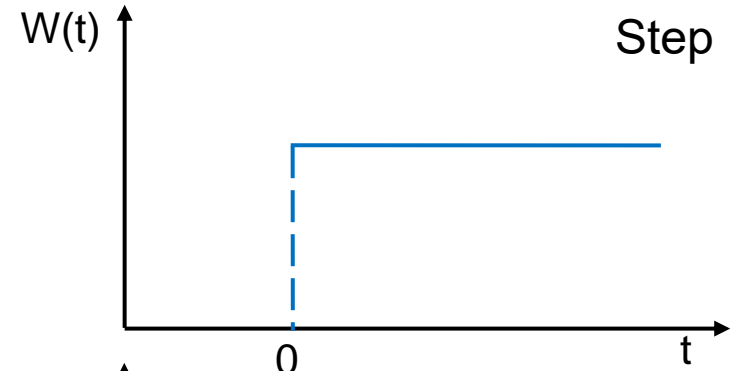
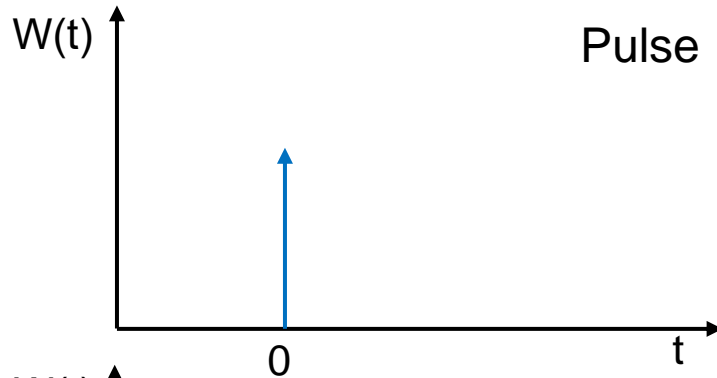
Response time	t_{50}	$T_{63.2}$	t_{75}	t_{90}	t_{95}	t_{99}
Formula	$0.693/\lambda$	$1/\lambda$	$1.39/\lambda$	$2.3/\lambda$	$3/\lambda$	$4.6/\lambda$

Example 3

For a lake has the following characteristics: volume = 50,000m³, depth = 2m, Inflow = outflow = 7500m³/day, temperature = 25⁰C, waste loading= 140,000g/day, Decay rate= 0.319 d⁻¹

- If the initial concentration is equal to a steady - state level (5.97 mg/l), determine the general solution.
- Determine the response time 75%, 90%, 95%, and 99%

❖ Particular solutions(c_p): Loading function



UNSTEADY- SYSTEMS SOLUTION (CONT)

❖ **Particular solutions:** Integrating factor method.

$$\frac{dy}{dx} + p(y)x = g(y)$$

$$I = e^{\int p(y)dy}$$

$$\frac{dc}{dt} + \lambda c = \frac{W(t)}{V}$$

$$I = e^{\int \lambda t} = e^{\lambda t}$$

$$e^{\lambda t} \frac{dc}{dt} + e^{\lambda t} \lambda c = e^{\lambda t} \frac{W(t)}{V}$$

$$\frac{d}{dt}(e^{\lambda t}c) = e^{\lambda t} \frac{dc}{dt} + e^{\lambda t} \lambda c$$

$$\frac{dc}{dt}(e^{\lambda t}c) = e^{\lambda t} \frac{W(t)}{V}$$

$$e^{\lambda t}c \Big|_0^t = \frac{1}{V} \int e^{\lambda t} W(t) dt$$

$$ce^{\lambda t} - c_0 = \frac{1}{V} \int e^{\lambda t} W(t) dt$$

$$c(t) = c_0 e^{-\lambda t} + \frac{e^{-\lambda t}}{V} \int e^{\lambda t} W(t) dt$$

 c_g
 c_p

UNSTEADY- SYSTEMS SOLUTION (CONT)

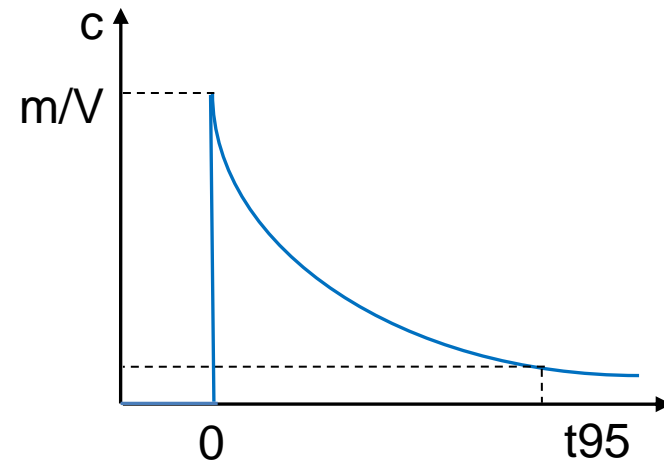
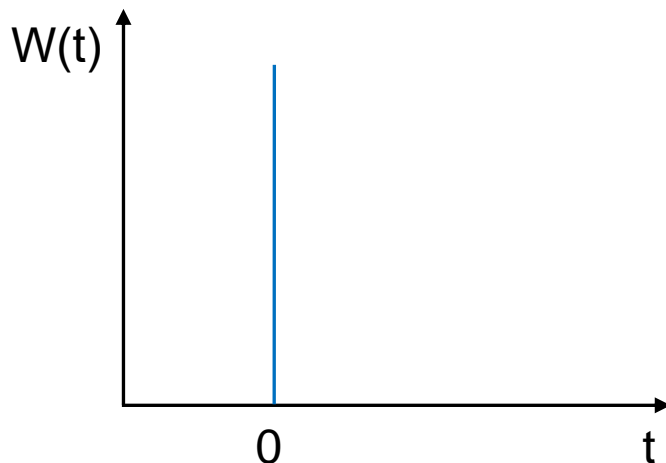
❖ IMPULSE LOADING (SPLII)

Describes the discharge that takes place in a short time.

Impulse function: $W(t) = m\delta(t)$ (m: quantity of pollutant mass[M])

$$\text{Equation(*)}: \frac{dc}{dt} + \lambda c = \frac{m\delta(t)}{V}$$

$$\text{Particular solution: } c = \frac{m}{V} e^{-\lambda t}$$



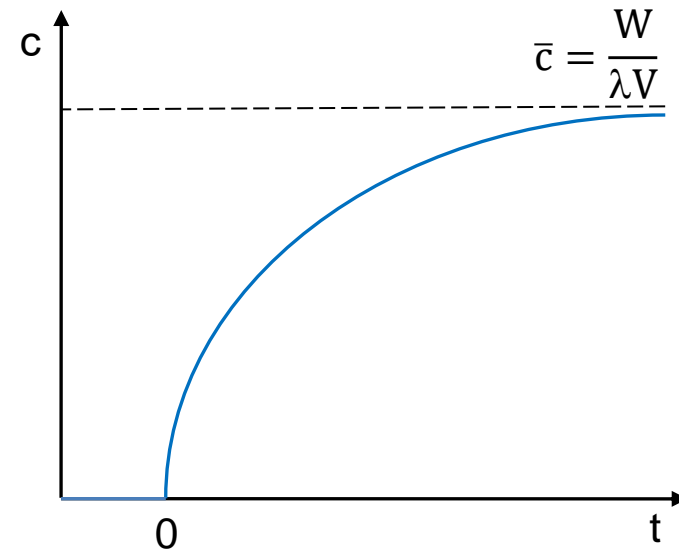
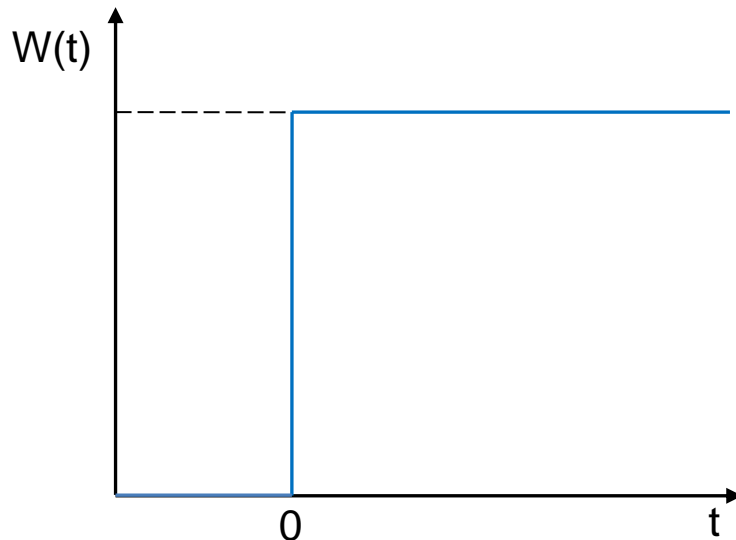
Plot of (a) loading and (b) response for impulse loading

UNSTEADY- SYSTEMS SOLUTION (CONT)

❖ Step loading (new continuous source)

❖ Step Function: $W(t) = \begin{cases} 0, & t < 0 \\ W, & t \geq 0 \end{cases}$ (W: Loading[MT⁻¹])

Particular solution : $c = \frac{W}{\lambda V} (1 - e^{-\lambda t})$



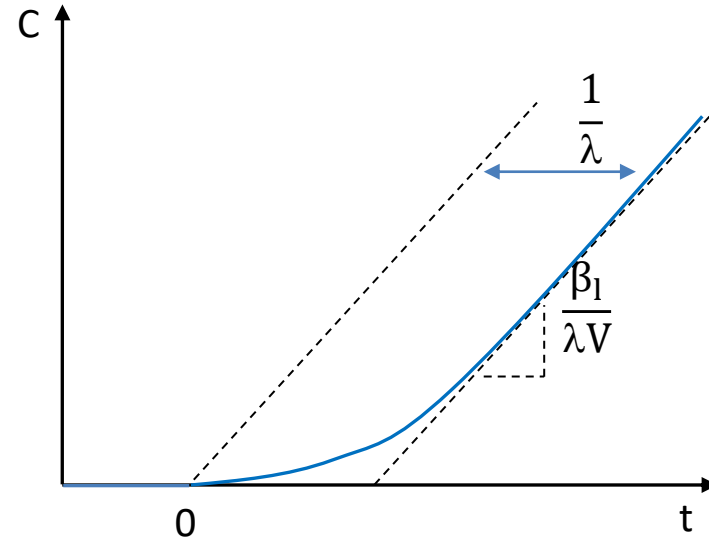
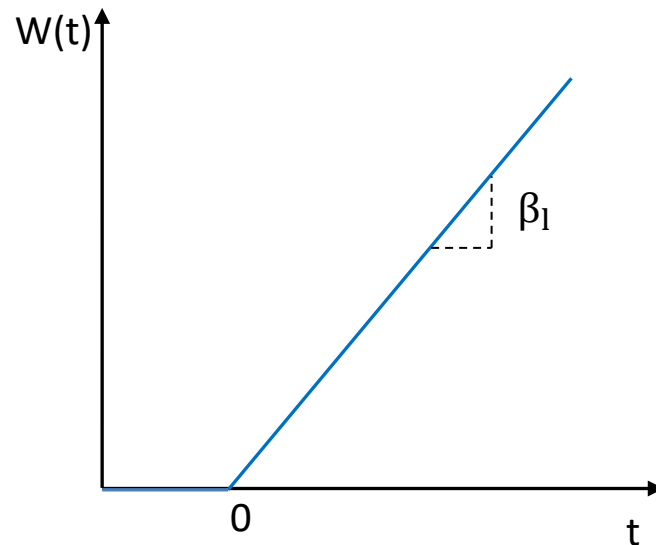
Plot of (a) loading and (b) response for impulse loading

UNSTEADY- SYSTEMS SOLUTION (CONT)

❖ Linear (Ramp) Loading

❖ Linear function: $W(t) = \pm\beta_l t$ (β_l : rate of change[MT^{-2}])

$$\text{Particular solution : } c = \pm \frac{\beta_l}{\lambda^2 V} (\lambda t - 1 + e^{-\lambda t})$$



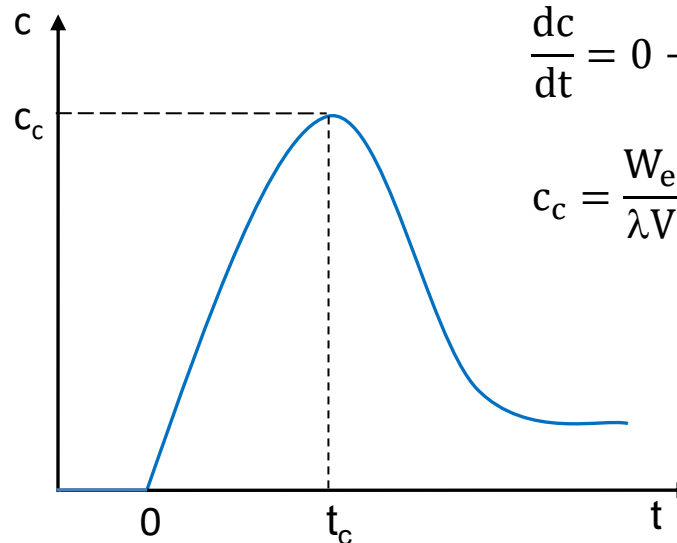
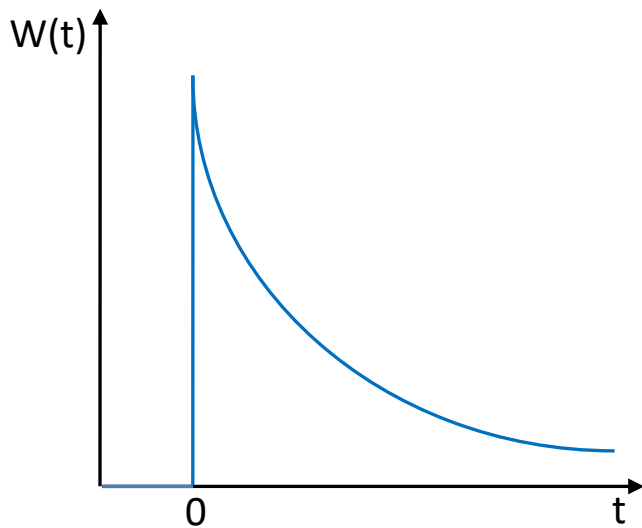
Plot of (a) loading and (b) response for a lineare increasing loading

UNSTEADY- SYSTEMS SOLUTION (CONT)

❖ Exponential loading

Exponential function: $W(t) = W_e e^{\pm\beta_e t}$ (W_e : a parameter that denote the value at $t = 0$ [MT^{-1}], β_e : growth rate (+) or decay (-) of loading [T^{-1}])

$$\text{Particular solution : } c = \frac{W_e}{V(\lambda \pm \beta_e)} \left(e^{\pm\beta_e t} - e^{-\lambda t} \right)$$



$$\frac{dc}{dt} = 0 \rightarrow t_c = \frac{\ln(\beta_e/\lambda)}{\beta_e - \lambda}$$

$$c_c = \frac{W_e}{\lambda V} e^{-\beta_e t_c} = \frac{W_e}{\lambda V} \left(\frac{\beta_e}{\lambda} \right)^{\frac{\beta_e}{\lambda - \beta_e}}$$

Plot of (a) loading and (b) response for an exponential decaying loading

Exercise 1:

A lake receives two sources of waste of a preserved pollutant from two plants with the following characteristics:

Source of waste from factory 1 with the load of pollutants with the following characteristics:

$$W(t) = \begin{cases} 0 & , x < 1930 \\ 13.2 \times 10^9(t - 1930) & , 1930 \leq t \leq 1960 \end{cases}$$

Waste source from factory 2 with pollutant load has the following characteristics:

$$W(t) = \begin{cases} 0 & , x < 1900 \\ 229 \times 10^9 e^{0.015(t-1900)} & , 1900 \leq t \leq 1960 \end{cases}$$

where $W(t)$ has units g/year

The initial concentration of the lake is 3mg/l. Characteristics of the lake: outflow $49.1 \times 10^9 \text{ m}^3/\text{year}$, $V = 4880 \times 10^9 \text{ m}^3$. Determine the concentration of pollutants in the lake from 1900 to 1960.

Solution:

Because chloride is a conservative substance.:

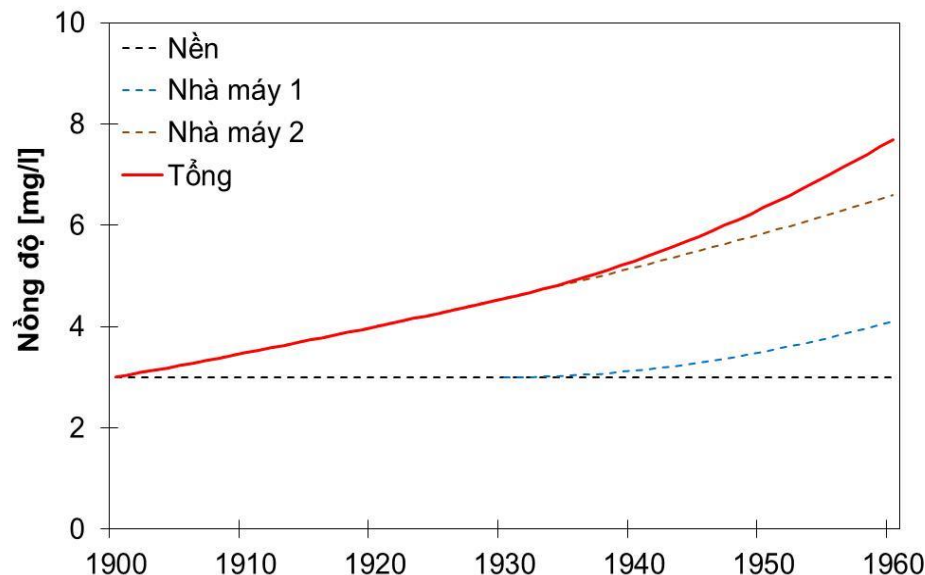
$$\lambda = \frac{Q}{V} = \frac{49.1 \times 10^9}{4880 \times 10^9} = 0.01 \text{ (yr}^{-1}\text{)}$$

From 1900 to 1930

$$c = 3 + \frac{229 \times 10^9}{4880 \times 10^9(0.01 + 0.015)} (e^{0.015(t-1900)} - e^{-0.01(t-1900)})$$

From 1930 to 1960

$$c = 3 + \frac{229 \times 10^9}{4880 \times 10^9(0.01 + 0.015)} (e^{0.015(t-1900)} - e^{-0.01(t-1900)}) + \frac{13.2 \times 10^9}{0.01^2 \times 4880 \times 10^9} (-1 + e^{-0.01(t-1930)} + 0.01(t - 1930))$$



Concentration movement over time

Exercise 2.

The lake has the following characteristics: Inflow = outflow = 5×10^5 m³/year, volume = 4×10^7 m³, surface area = 5×10^6 m². The initial concentration of the lake in a stable state is 5 μg/l.

The lake receives two sources of waste as follows.:

- In 1994 the lake received a load of 500 kg/year from a fertilizer factory.
- In 1997, the lake began receiving waste from residential areas at a rate of population growth each year. $p = 200e^{0.2t}$ and each citizen will generate phosphorus amounts of 0.5 kg per year.

Calculate the concentration of the lake from 1994 to 2010. Know the deposition speed of phosphorus is 8m /year.